Astronomical Techniques II Lecture 3 - Noise, Temperature and SNR

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March-May 2014

Spectral Power

$$W = \int_{\nu} \int_{aperture} \int_{\Omega} B(\theta, \phi, \nu) \cos\theta dA \ d\Omega \ d\nu \quad W$$

$$w_{
u} = \int_{aperture} \int_{\Omega} B(\theta, \phi, \nu) \cos \theta dA \ d\Omega \ W \ Hz^{-1}$$

$$w_{
u} = A_{eff} \int_{\Omega} B(\theta, \phi, \nu) \cos \theta \ d\Omega \ W \ Hz^{-1}$$

$$w_{
u} = A_{eff} \int_{\Omega} B(heta, \phi,
u) \ P(heta, \phi,
u) \ d\Omega \ W \ Hz^{-1}$$

For a uniform source of Brightness B_u , this becomes $w_{\nu} = \frac{1}{2} A_{eff} B_u \Omega_A \quad W Hz^{-1}$

Spectral Power

$$w_{
u} = A_{eff} \int_{\Omega} B(\theta, \phi, \nu) P(\theta, \phi, \nu) d\Omega \quad W Hz^{-1}$$

Cross-correlation form:

$$w_{\nu} = A_{eff} \int_{\Omega} B(\theta, \phi, \nu) P(\Omega - \Omega_0, \nu) d\Omega \quad W Hz^{-1}$$

Convolution form:

$$w_{\nu} = A_{eff} \int_{\Omega} B(\theta, \phi, \nu) \tilde{P}(\Omega_0 - \Omega, \nu) \ d\Omega \quad W \ Hz^{-1}$$

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Planck's Law





4/13

Planck's and Rayleigh-Jeans Law

$$B_{\nu} = \frac{2h\nu^{3}}{c^{2}} \frac{1}{e^{h\nu/kT} - 1}$$
$$B_{\nu} = \frac{2kT\nu^{2}}{c^{2}} \frac{\frac{h\nu}{kT}}{e^{h\nu/kT} - 1}$$

Limit $h\nu << kT$ Rayleigh-Jeans Law

$$B_{\nu} = rac{2kT}{\lambda^2} W m^{-2} sr^{-1} Hz^{-1}$$

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Power received at a detector

$$dW = B(heta, \phi,
u) \ cos heta dA \ d\Omega \ d
u$$

 dW - W
 $B(heta, \phi) - W \ m^{-2} \ sr^{-1} \ Hz^{-1}$

Practical quantitative definition

$$B(\theta, \phi, \nu) = \frac{dW}{d\Omega \cos\theta dA \ d\nu} = \frac{2kT}{\lambda^2}$$

- Intrinsic property of the source
- Independent of the distance from the source (ONLY for a resolved object)
- Can be thought of as energy *received* at the detector OR as energy *emitted* by the source.

Brightness and Temperature

$$S = \frac{2kT\Omega_s}{\lambda^2}$$

$$S = \frac{2k}{\lambda^2} \int_{\Omega_s} T(\theta, \phi) \ d\Omega$$

$$S = rac{2k}{\lambda^2} \int_{\Omega_s} T(\theta, \phi) P(\theta, \phi) d\Omega$$

- Associate a unique temperature with the power received at any given frequency. A property of the source.
- Represents the temperature of a Blackbody which would have given out exactly as much radiation at that frequency (W m⁻² sr⁻¹ Hz⁻¹).
- For thermal radiation from an optically thick source same as the physical temperature of the body emitting the radiation.
- For non-thermal radiation eq. radiation temperature

7/13

Noise power measured per unit bandwidth at the terminals of a resistance R at temperature T (Nyquist, 1928) $w = kT W Hz^{-1}$

load \rightarrow lossless antenna of radiation resistance R, the impedence as seen at the terminals is unchanged.

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8/13

The noise spectral power received by the antenna

$$w = \frac{1}{2} A_{eff} \int_{\Omega} B(\theta, \phi) P(\theta, \phi) d\Omega$$
$$w = \frac{k A_{eff}}{\lambda^2} \int_{\Omega} T(\theta, \phi) P(\theta, \phi) d\Omega W Hz^{-1}$$

Antenna Temperature

The temperature of antenna radiation resistance



Fig. 3-24. (a) Resistor at temperature T; (b) antenna in an absorbing box at temperature T; and (c) antenna observing sky of temperature T. The same noise power is available at the terminals in all three cases.

$$w = \frac{1}{2} A_{eff} \int_{\Omega} B(\theta, \phi) P(\theta, \phi) d\Omega = kT$$

Recall that

$$S = \int_{\Omega} B(\theta, \phi) P(\theta, \phi) d\Omega$$
$$\implies S = \frac{2kT}{A_{eff}}$$
$$T_A = \frac{A_{eff}}{\lambda^2} \int_{\Omega} T_s(\theta, \phi) P(\theta, \phi) d\Omega$$
$$T_A = \frac{1}{\Omega_A} \int_{\Omega} T_s(\theta, \phi) P(\theta, \phi) d\Omega$$

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Antenna Temperature

The compact source and extended source cases.

Noise and Signal

- Signal *T_{Ant}* what comes from the sky
- Noise everything else
 - Receiver T_{Rec}
 - Spillover T_{Spill}
 - Leakage T_{Leak}
 - Loss T_{Loss}
 - Radio Frequency Interference (RFI)

$$T_{Sys} = T_{Ant} + T_{Rec} + T_{Spill} + T_{Leak} + T_{Loss}$$

- The signal has the same characteristics as noise
- One is looking for an increase of T_{Ant} over a background of T_{Sys}.

Minimum Detectable Signal

$$\Delta T_{min} = \frac{T_{Sys}}{\sqrt{\Delta\nu\Delta\tau}}$$
$$\Delta B_{min} = \frac{2k}{\lambda^2} \frac{T_{Sys}}{\sqrt{\Delta\nu\Delta\tau}}$$
$$\Delta S_{min} = \frac{2k}{A_{Eff}} \frac{T_{Sys}}{\sqrt{\Delta\nu\Delta\tau}}$$

- In theory, can be reduced to an arbitrarily small number by increasing the denominator.
- In practice:
 - Limited Δt source evolution, source visibility, system stability, TAC, human effort
 - Limited Δν spectral signature (emission/absorption lines, EoR), source evolution, instrumental capability, technical challenges